

Petrophysical Services (Calgary) Limited  
137 Cranleigh Bay SE., Calgary, Alberta T3M 1h5  
(403) 271-7930 email wfcLOW@shaw.ca

### **Log Analysis Report Kola Pool, Bakken**

Petrophysical Services was requested to analyze 30 wells over the Bakken sand in the Kola pool, TWP 10 R 29W1. As there is potential in the Lodgepole in the area, the Lodgepole was also analysed.

For the Bakken, formation water resistivity (rw) used was 0.05 @ 25C, which corresponds to a salinity of ~160k ppm NaCl. For the Lodgepole, initial rw used was 0.12 @ 25C. Based on some recent work in the Lodgepole in TWP 10 R 28, rw was changed to 0.065 @ 25C, ~118,000 ppm NaCl.

#### **Method:**

Log data was generally digitized by Divestco. Core analysis was acquired from Geoscout, resampled to 0.1m, and plotted against the log analysis results. Although log analysis was not adjusted to match core data, there is generally a pretty good comparison between the log analysis results and the core data.

**a) Shale Volume** was calculated from gamma ray using linear formula over the Lodgepole, and using clavier formula over the Bakken. 0% shale for the Bakken was generally picked high, 60 to 80 api, compared to the Lodgepole pick.

**b) Porosity** was calculated from shale corrected neutron density crossplot, or from sonic, depending on availability.

**c) Water Saturation** was calculated using the Archie formula with  $a = 1$ ,  $m = 2$  and  $n = 2$  over the Lodgepole, and from NQv, a variation of dual water, with  $a = 1$ ,  $m = 1.8$  and  $n = 2$  over the Bakken.

Irreducible water saturation was estimated using  $\Phi * S_w = 0.08$ . SWIR is used as a guide to predicting water producing zones.

**d) Lithology** was calculated from apparent grain density.

**e) Net pay** was calculated using porosity, saturation, shale volume cutoffs. Pay flag (black) is based on  $\Phi \geq 9\%$ ,  $S_w \leq 60\%$  and  $VSH \leq 40\%$ . Reservoir flag (red) is based on  $\Phi \geq 9\%$  and  $VSH \leq 40\%$ .

Regards

W. F. (Bill) Clow, P. Eng.

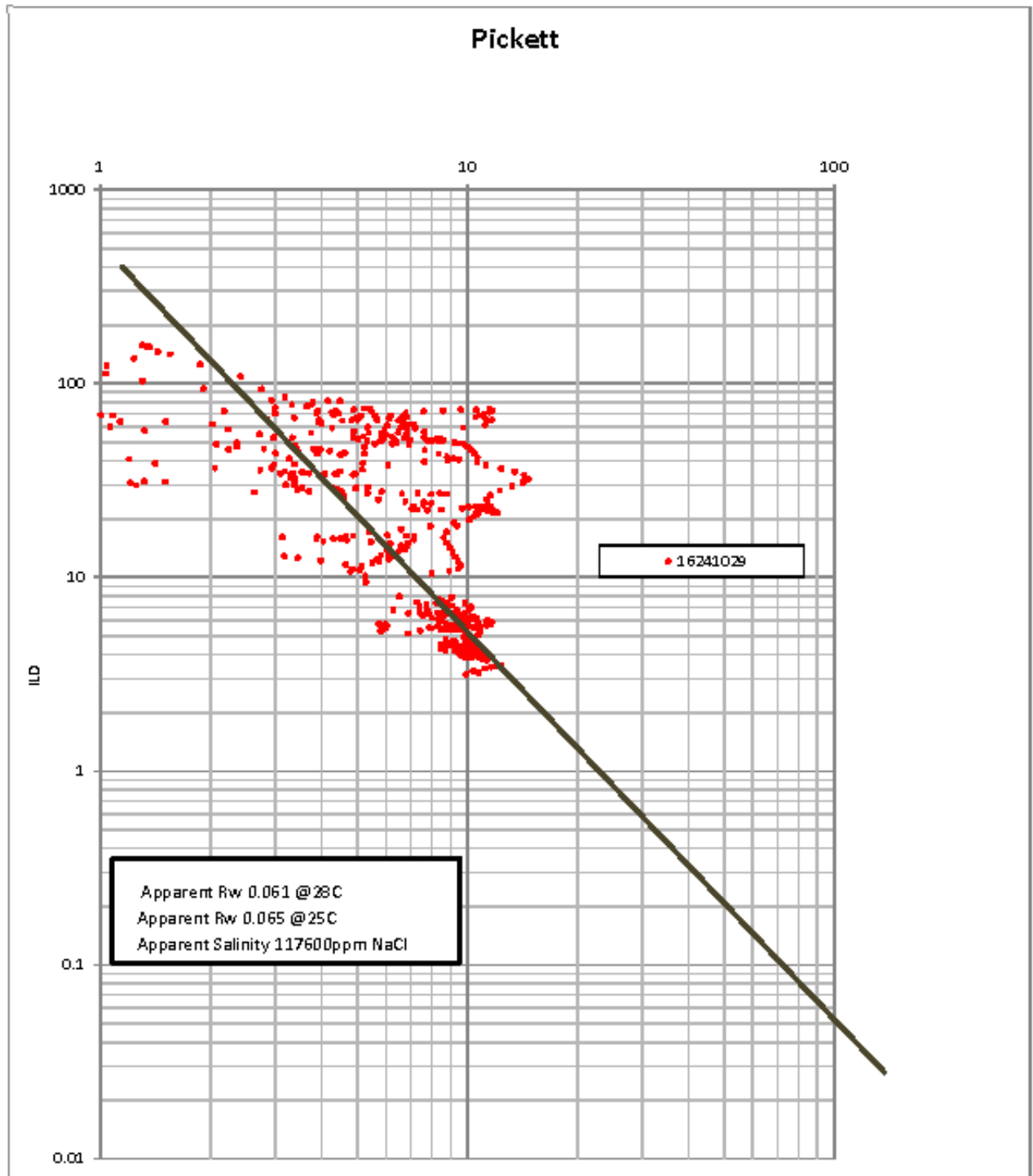


Figure 1 Pickett plot, Lodgepole 16-24-10-29W1

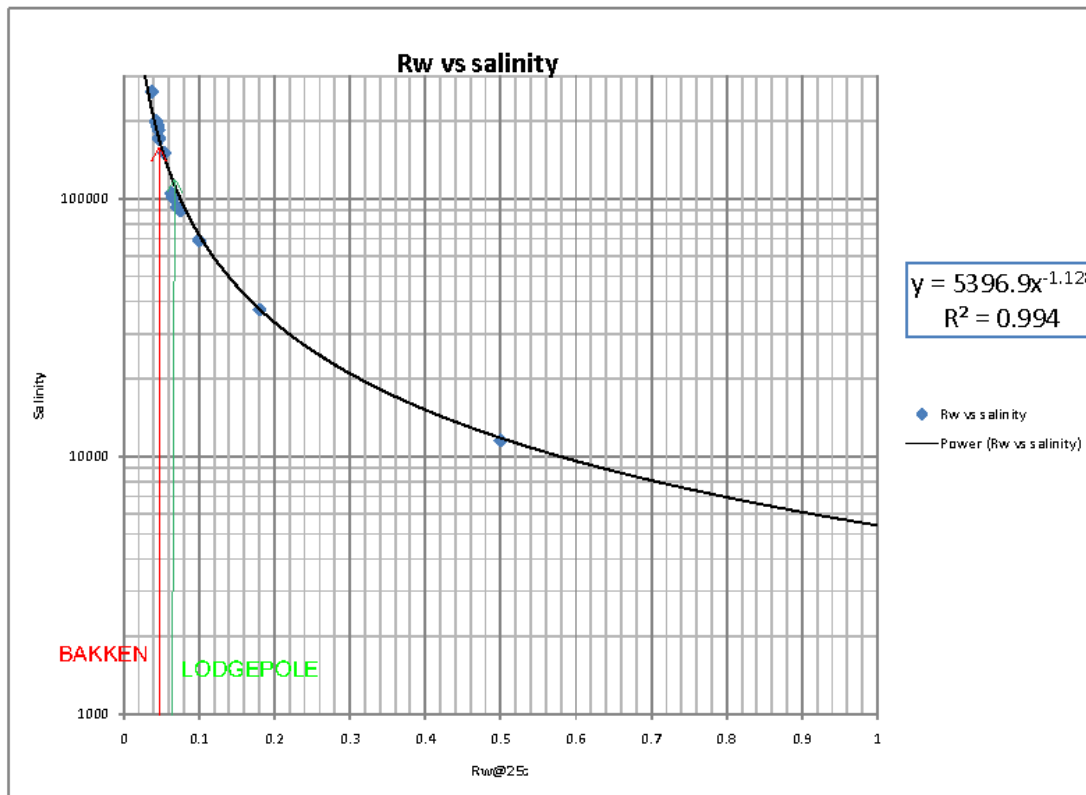


Figure 2 Rw vs salinity

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Lodgepole parameters (typical)

SHALE FROM: GAMMA RAY LINEAR  
15 Gamma Ray clean (api) = 20  
16 Gamma Ray Shale (api) = 100  
17 clay content multiplier = 1  
18 material balance for vshale <Y/N> = Y  
POROSITY FROM: NEUTRON/DENSITY CROSSPLOT  
22 Limestone or Sandstone porosity units = L  
20 Neutron Porosity shale (%) = 30  
21 Density Porosity shale (%) = 12  
32 default matrix density (K/M3) = 2700  
23 default fluid density (K/M3) = 1000  
141 limit dens phi to nphi + = .02  
111 use sonic to limit porosity = N  
24 material balance for porosity = Y  
25 maximum porosity (%) = 30  
COAL LOGIC:  
103 coal logic level = 0  
104 coal if phin greater than = .4  
105 coal if dens less than = 2000  
106 coal if delt greater than = 450  
BAD HOLE LOGIC:  
99 bad hole logic level = 0  
100 caliper limit (mm) = 330  
101 density porosity limit = .2  
102 neutron porosity limit = .3  
LITHOLOGY FROM: Apparent Grain Density  
48 density of SANDSTONE (K/M3) = 2650  
49 density of LIMESTONE (K/M3) = 2710  
50 density of DOLOMITE (K/M3) = 2870  
51 density of ANHYDRITE (K/M3) = 2970  
52 density of SALT (K/M3) = 1500  
53 density of GYPSUM (K/M3) = 2200  
54 minimum volume cutoff = .1  
175 fractional anhydrite = Y  
WATER SATURATION FROM: ARCHIE  
68 tortuosity constant = 1  
36 cementation exponent = 2  
38 saturation exponent = 2  
69 water resistivity (ohmm) = .12  
70 rw temperature (degC) = 25  
4 surface temperature (deg C) = 4  
5 maximum temperature (deg C) = 30  
6 depth of maximum temperature (m) = 900  
71 material balance for sw <Y/N> = Y  
PERM FROM: Morris/Biggs  
74 hydrocarbon type: Oil or Gas = 0  
75 Buckles # for 0\*SWirr = .06  
PAY FLAG CRITERIA:  
173 results by weight? = N  
94 porosity cutoff (frac) = .09  
95 water saturation cutoff (frac) = .6  
96 permeability or weight cutoff (md) = 0  
97 shale volume cutoff (frac) = .4  
98 depth limit (m) = 5000

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**Bakken parameters (typical)**

SHALE FROM: GAMMA RAY CLAVIER  
15 Gamma Ray clean (api) = 50  
16 Gamma Ray Shale (api) = 140  
17 clay content multiplier = 1  
18 material balance for vshale <Y/N> = Y  
POROSITY FROM: NEUTRON/DENSITY CROSSPLOT  
22 Limestone or Sandstone porosity units = L  
20 Neutron Porosity shale (%) = 30  
21 Density Porosity shale (%) = 15  
32 default matrix density (K/M3) = 2700  
23 default fluid density (K/M3) = 1000  
141 limit dens phi to nphi + = 0  
111 use sonic to limit porosity = N  
24 material balance for porosity = Y  
25 maximum porosity (%) = 30  
COAL LOGIC:  
103 coal logic level = 0  
104 coal if phin greater than = .4  
105 coal if dens less than = 2000  
106 coal if delt greater than = 450  
BAD HOLE LOGIC:  
99 bad hole logic level = 0  
100 caliper limit (mm) = 330  
101 density porosity limit = .2  
102 neutron porosity limit = .3  
LITHOLOGY FROM: Apparent Grain Density  
48 density of SANDSTONE (K/M3) = 2650  
49 density of LIMESTONE (K/M3) = 2710  
50 density of DOLOMITE (K/M3) = 2870  
51 density of ANHYDRITE (K/M3) = 2970  
52 density of SALT (K/M3) = 1500  
53 density of GYPSUM (K/M3) = 2200  
54 minimum volume cutoff = .1  
175 fractional anhydrite = Y  
WATER SATURATION FROM: NORMALIZED QV  
68 tortuosity constant = 1  
36 cementation exponent = 1.8  
38 saturation exponent = 2  
69 water resistivity (ohmm) = .05  
70 rw temperature (degC) = 25  
4 surface temperature (deg C) = 4  
5 maximum temperature (deg C) = 30  
6 depth of maximum temperature (m) = 900  
72 shale resistivity (ohmm) = 2  
73 shale porosity coefficient = 1  
142 use ress for resd <Y/N> = N  
71 material balance for sw <Y/N> = Y  
PERM FROM: Morris/Biggs  
74 hydrocarbon type: Oil or Gas = 0  
75 Buckles # for 0\*SWirr = .08  
PAY FLAG CRITERIA:  
173 results by weight? = N  
94 porosity cutoff (frac) = .09  
95 water saturation cutoff (frac) = .6  
96 permeability or weight cutoff (md) = 0  
97 shale volume cutoff (frac) = .4  
98 depth limit (m) = 5000